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Wavelet decomposition of forced turbulence: Applicability of the iterative Donoho-Johnstone threshold

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We examine the decomposition of forced Taylor-Green and Arn'old-Beltrami-Childress (ABC) flows into coherent and incoherent components using an orthonormal wavelet decomposition. We ask whether wavelet coefficient thresholding based on the Donoho-Johnstone criterion can extract a coherent vortex signal while leaving behind Gaussian random noise. We find that no threshold yields a strictly Gaussian incoherent component, and that the most Gaussian incoherent flow is found for data compression lower than that achieved with the fully iterated Donoho-Johnstone threshold. Moreover, even at such low compression, the incoherent component shows clear signs of large-scale spatial correlations that are signatures of the forcings used to drive the flows. © 2012 American Institute of Physics. [http://dx.doi.org/10.1063/1.3683556]

I. INTRODUCTION

Previous work has explored the application of the discrete wavelet transform to two- and threedimensional turbulence simulation data in an effort to segregate the flow into distinctly different components based on wavelet amplitudes (e.g., Refs. 1–3). Farge *et al.*^{1,2} refer to this process as coherent vortex extraction (CVE), reflecting the conjecture that turbulent flows are composed of coherent structures that dominate at energy bearing scales and an incoherent background component which can be modeled as Gaussian random noise. Segregation relies on application of a wavelet amplitude threshold. The one generally employed is the universal threshold of Donoho and Johnstone.⁴ This threshold is simple to employ and minimizes the maximum error in the signal in the presence of additive and uncorrelated Gaussian noise when the noise variance is known. As the noise variance is not known *a priori* for a turbulent flow, CVE relies on an iterative scheme⁵ to estimate it.

Application of the CVE methodology has led to the identification of two apparent components in simulated turbulent flows: one reconstructed from a small percentage of the highest amplitude wavelet coefficients, called coherent and more generally considered signal, and the other reconstructed from the remaining coefficients, called incoherent and more generally considered noise. The coherent component has properties similar to the original flow. It contains ~99% of the kinetic energy of the unfiltered flow, has a relative kinetic helicity distribution $h = \frac{u \cdot \omega}{|u||\omega|}$ which peaks near ± 1 , as the original flow being examined, and shows a $k^{-5/3}$ kinetic energy spectrum through the inertial range. The incoherent component, by contrast, typically contains less than 1% of the flow energy, shows a peak in its helicity distribution near h = 0, and exhibits a k^2 kinetic energy spectrum.^{2,3}

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025102-2 Lord et al.

In this paper, we report on the results of wavelet analysis of two 1024^3 simulations of turbulence forced coherently at large scale, one as a Taylor-Green (TG) and the other as an Arn'old-Beltrami-Childress (ABC) flow (Eqs. (3) and (4) below). We examine sensitivity to three different wavelets, apply threshold filtering to either the magnitude of the vorticity or the amplitudes of the individual components independently, and study compression ratios ranging from 10% to 98.7%, the later achieved when the iterative Donoho-Johnstone threshold is applied to the wavelet amplitudes of the individual vorticity components. We find, independent of the wavelet or thresholding scheme employed, that the gross properties of the coherent flow component are similar to those reported in previous CVE studies, and additionally that it maintains the temporal correlations of the original flow. In contrast to previous work, however, we find that the incoherent flow component shows a k^2 spectrum only when the threshold filter is applied to the individual vorticity components, not when it is applied to the vorticity magnitude as in previous studies, and when it occurs, the k^2 scaling extends only over a small range of high wavenumbers. Moreover, although the incoherent flow displays short temporal correlation, as would be expected for random noise, the statistics at any single time are significantly non-Gaussian. We examine this non-Gaussianity for a range of filter thresholds and find that it persists to very low compression values. Further, we demonstrate that, even at low compression, the incoherent component shows spatial correlations which reflect the large-scale properties of the original flow and thus contains some residual signal that cannot be characterized as random noise.

This paper is organized as follows. In Sec. II, we describe the forced Taylor-Green and ABC flow simulation solutions we analyze. In Sec. III, we briefly summarize the CVE method as we apply it, and in Sec. IV present the results of that analysis. In Sec. V, we look at the single-point statistics of the incoherent component more closely to determine if they are Gaussian, and examine the degree of Gaussianity as a function of compression. We also examine the point-wise helicity distributions to determine if important vector alignments are preserved. Finally, in Sec. VI, we extend the analysis to include correlations within the flows to understand the spatial structure and temporal persistence of both the coherent and incoherent components, before concluding our discussion in Sec. VII.

II. FORCED TURBULENCE SIMULATIONS

We examine two flows resulting from direct numerical simulation of the forced incompressible Navier-Stokes equations,⁶

$$\partial_t \boldsymbol{u} + \boldsymbol{u} \cdot \nabla \boldsymbol{u} = -\nabla p + \nu \nabla^2 \boldsymbol{u} + \boldsymbol{f},\tag{1}$$

and

$$\nabla \cdot \boldsymbol{u} = \boldsymbol{0},\tag{2}$$

where u is the velocity, p is the pressure, v is the kinematic viscosity, and f is an applied specific body force, and the fluid density $\rho = 1$ without any loss of generality. The equations are discretized pseudo-spectrally, employing 2/3 de-aliasing (maximum wavenumber $k = k_{max} = N/3$) (Ref. 7) in a triply periodic domain with N = 1024 grid points in each of the three directions, and time advanced using a second order Runga-Kutta scheme. The domain size is specified as 2π in each direction and the values of f and v chosen so that the solution has rms velocity amplitude $U \sim 1$ and Kolmogorov dissipation wavenumber less than k_{max} . The time step $\Delta t = 7.5 \times 10^{-4}$ then meets the Courant-Friedricks-Lewy criterion on the grid with a safety factor of about 0.8. The resulting solutions are thus well resolved; the dissipative wavenumber is smaller than k_{max} at all time steps. The product of k_{max} and the Kolmogorov dissipation scale, $\eta = (v^3/\epsilon)^{1/4}$ with ϵ the energy injection rate, is 1.2 for both simulations.

The simulations differed primarily in the body force applied. One employed a Taylor-Green form

$$f_{TG} = f_0[\sin(k_F x)\cos(k_F y)\cos(k_F z)\hat{x} - \cos(k_F x)\sin(k_F y)\cos(k_F z)\hat{y}], \qquad (3)$$

with $k_F = 2$. Taylor-Green forcing does not introduce net kinetic helicity into the flow. For the particular simulation run analyzed, the viscosity in Eq. (1) was set to $v = 3 \times 10^{-4}$ and the amplitude of the forcing to $f_0 = 0.377$. These values led, in the turbulent steady state, to solutions with rms velocity amplitude $U \sim 1$. The computed flow has an integral-scale Reynolds number of Re = 3950 and a Taylor-scale Reynolds number of $R_{\lambda} = 800$.

The second simulation implemented ABC forcing

$$f_{ABC} = f_0 \{ [B \cos(k_F y) + C \sin(k_F z)] \hat{x} + [A \sin(k_F x) + C \cos(k_F z)] \hat{y} + [A \cos(k_F x) + B \sin(k_F y)] \hat{z} \},$$
(4)

with $k_F = 3$, A = 0.9, B = 1, and C = 1.1. The ABC forcing does introduce net positive helicity, with an helicity injection rate, normalized by the injection wavenumber, equal to the energy injection rate, $\tilde{\epsilon}/k_F \sim \epsilon \sim 0.25$, and yielding a nearly maximally helical flow; the mean relative helicity of the solution fluctuates around a value of ~ 0.75 . In this simulation the viscosity in Eq. (1) was set to $\nu = 2.5 \times 10^{-4}$, and the amplitude of the forcing to $f_0 = 0.115$, which also led, in the turbulent steady state, to solutions with rms velocity amplitude $U \sim 1$. The computed flow in this case has somewhat higher integral-scale and Taylor-scale Reynolds numbers, Re = 6200 and $R_{\lambda} = 1100$, respectively.

The Reynolds numbers quoted above are defined as follows. The integral-scale Reynolds number is Re = UL/v, where L is the integral scale of the flow obtained from the energy spectrum E(k) as

$$L = 2\pi \frac{\int E(k)k^{-1}dk}{\int E(k)dk}.$$
(5)

The factor 2π comes from the fact that our computational domain has length 2π , and we use integer wavenumbers in Fourier space. The Taylor-scale Reynolds number is similarly $Re = U\lambda/\nu$, where λ is the Taylor length scale given by

$$\lambda = 2\pi \left[\frac{\int E(k)dk}{\int E(k)k^2dk} \right]^{1/2}.$$
(6)

III. COHERENT VORTEX EXTRACTION

We examine the simulation solutions using the multiresolution wavelet analysis and thresholding techniques of Farge *et al.*^{1,2,5} to separate the flow based on its vorticity into the previously mentioned coherent (signal) and incoherent (noise) components. The CVE method consists of three steps [e.g., Ref. 8:

- 1. Decomposition: An orthogonal wavelet transform of each vector component of the vorticity, $\boldsymbol{\omega} \equiv [\omega_x, \omega_y, \omega_z]$, yields the wavelet coefficient vector $\tilde{\boldsymbol{\omega}}$, the projection of the vorticity in wavelet space.
- 2. Thresholding: A filter is applied to the wavelet coefficients based on the magnitude of the vorticity vector. The threshold amplitude A_{DJ} is taken to be the "universal threshold" of Ref. 4

$$A_{\rm DJ} = \sqrt{\frac{4}{3}Z\ln N} , \qquad (7)$$

where *N* is the total number of data points and $Z \equiv \frac{1}{2} \langle \boldsymbol{\omega} \cdot \boldsymbol{\omega} \rangle$ is the enstrophy of the flow; *Z*/3 is one-half the average variance of the three vorticity vector components when their means are zero. The incoherent (noise) component of the flow is then composed of those wavelet coefficient vectors with magnitude below the threshold value and the coherent (signal) component of those with magnitudes that exceed it. Since the universal threshold is defined in terms of the variance of the noise, and since the variance of the incoherent vorticity (noise

025102-4 Lord et al.

component) is not known *a priori* and is, in general, not equal to the enstrophy of the full flow, Eq. (7) provides only a first estimate of the threshold value. It is refined iteratively⁵ by successive evaluation of Eq. (7) using the enstrophy of the incoherent component after filtering based on the previous threshold. The iteration converges when the variance of the incoherent vorticity becomes stationary; when there is no change in the assignment of the coefficients as coherent or incoherent. This generally occurs after about 35 iterations.

Unlike previous work, we also examine a filtering scheme which employs the same filter threshold but applies it to each vorticity component separately and independently, based on their individual amplitudes. This iteratively converges to somewhat different results, primarily because it yields higher flow compression (Sec. IV), compressions more in line with those achieved by the application of a threshold based on a single iteration to the vorticity magnitude.^{8–10}

3. Reconstruction: The coherent vorticity ω_C is reconstructed by the inverse wavelet transform of the wavelet vectors with magnitudes above the threshold value, or in the case of the filter being applied to the components, by the inverse transform of the wavelet coefficients with individual amplitudes that exceed the threshold value. Since the wavelets employed are orthonormal, the incoherent component ω_I can be reconstructed either by inverse transformation of the low magnitude wavelet vectors or low amplitude coefficients, or by subtracting the coherent component from the original vorticity; $\omega_I = \omega - \omega_C$.

The data compression achieved by this process is defined as the fraction of coefficients used to construct the incoherent component, or equivalently the fraction considered noise and thus not needed in reconstruction of the signal (the coherent component approximation to the original flow).

Finally, the coherent and incoherent flow velocities are reconstructed from the corresponding vorticities via a spectral inverse curl. We note that the wavelet decomposition introduces signal above the Orszag frequency k_{max} into both the coherent and incoherent components. The total power in the wavelet coefficients is preserved (incoherent and coherent contributions above k_{max} sum to zero), but the spectra of the filtered components individually reflect this redistribution (Figure 3).

IV. CVE ANALYSIS OF TAYLOR-GREEN AND ABC FLOWS

The most important findings from previous CVE decompositions of turbulent flow are:

- 1. Using less than 2.6% of the wavelet coefficients in the reconstruction of the coherent vorticity yields a flow with nearly all (99.8%) of the kinetic energy and most of (79.8%) the enstrophy of the original flow.⁹
- 2. The incoherent vorticity has low amplitude and is described as spatially random, structureless, and non-intermittent, though it displays an exponential distribution of values. The incoherent velocity is nearly Gaussianly distributed with very small variance.^{2,9,11,12}
- 3. The relative kinetic helicity distribution of the incoherent component has the opposite curvature to that of the original, peaking near h = 0 rather than at ± 1 as that of the original flow.^{2,3,12}
- 4. The kinetic energy spectrum of the coherent flow matches that of the original from the integral scale through the inertial range where it follows $k^{-5/3}$; differences between the spectra are confined to the dissipative range. The incoherent component, on the other hand, shows k^2 spectrum, with a peak at the low wave number end of the dissipative range where it joins the original flow spectrum.^{2,3,9,12}

These findings largely result from Coifman12 wavelet analysis of both run-down and forced turbulent flows, though the results are reported to be robust to the choice of orthogonal wavelet, excluding the Haar,⁹ but not to biorthogonal decomposition.¹² Here we investigate the effectiveness of CVE when employing the Haar, Coifman12, and Coifman30 wavelets in the analysis of Taylor-Green and ABC flows.

The gross properties of our CVE results are similar to those previously published, but as summarized in Table I, the compressions we achieve when applying the iterative Donoho-Johnstone

Forcing	Wavelet	Compression (%)		Kinetic energy retained (%)		Enstrophy retained (%)	
		$ \omega $	$ \omega_{x, y, z} $	$ \omega $	$ \omega_{x, y, z} $	$ \omega $	$ \omega_{x, y, z} $
Taylor-Green	Haar	94.5	98.6	98.8	97.2	90.4	80.8
Taylor-Green	Coifman12	91.8	97.6	99.98	99.8	98.1	94.9
Taylor-Green	Coifman30	91.3	97.4	99.99	99.9	98.7	96.1
Arn'old-Beltrami-Childress	Haar	94.6	98.7	99.1	97.9	89.7	79.8
Arn'old-Beltrami-Childress	Coifman12	92.0	97.7	99.97	99.9	97.9	94.4
Arn'old-Beltrami-Childress	Coifman30	91.4	97.4	99.99	99.9	98.5	95.7

TABLE I. Compression achieved and kinetic energy and enstrophy retained in the coherent component of the flow after employing the iterative Donoho-Johnstone filter threshold on two-flows with three wavelets. Results differ when application of the filter is based on the vorticity magnitude $|\omega|$ vs. component amplitudes $|\omega_{x,y,z}|$.

threshold to the vorticity vector magnitude are significantly lower than those previously reported in the literature. Consequently, our decompositions also show greater retention of the flow kinetic energy and enstrophy by the coherent component. This decreased compression is likely due to our using a fully iterated threshold value rather than that obtained by a single iteration as in most previous work [cf. Ref. 9]. We explicitly employ the fully iterative scheme as we aim to focus on the statistical properties of the incoherent component in relationship to the Donoho-Johnstone threshold. Since the compression (as we have defined it) monotonically decreases with the number of iterations,⁹ the fully iterated incoherent variance will likely lie closest to that of the assumed uncorrelated Gaussian noise on which the universal threshold is based. We have applied single iteration thresholds, and then obtain similar compressions (e.g., 97.3% using the Coifman12 wavelet on the TG flow, and symbols with superimposed crosses in Figure 4) to those published. We also obtain higher compression ratios, similar to those of previous single iteration studies, when we apply the fully iterated threshold to individual vorticity component amplitudes rather than the vorticity vector magnitude. In those cases, the kinetic energy and enstrophy retained by the coherent flow are also reduced (Table I). For any of the threshold determination schemes, we find, as previous authors, that the gross properties of the coherent velocity and vorticity distributions are in good qualitative agreement with those of the unfiltered flow (Figure 1). We defer a quantitative assessment of the incoherent distributions to Sec. V A. There we motivate even weaker compression of the signal than that achieved by application of the iterative Donoho-Johnstone threshold.

The detailed coherent and incoherent Taylor-Green and the ABC kinetic helicity and kinetic energy distributions are similarly sensitive to the filter threshold. While the original flows and their coherent components show relative helicity distributions similar to those reported in earlier studies when the flows are well resolved and have little mean strain,^{13–15} peaking weakly near $h = \pm 1$, the incoherent flow components typically display an helicity maximum near h = 0 as in previous CVE studies (Figure 2). We note, however, that the incoherent ABC helicity distribution remains asymmetric, showing weak residual net helicity introduced by the forcing even at very low wavelet compression. Additionally, while the coherent flow kinetic energy spectra qualitatively match those of the original flows through the dissipative range and the incoherent power spectra peak at high k values (Figure 3), the latter show the k^2 scaling reported in previous CVE studies only when the filter is based on individual vorticity amplitudes rather than the vector magnitude, and even then over only a very limited range of wavenumbers. This again likely reflects the increased compression achieved in our work when the fully iterated threshold is applied to the vorticity wagnitude. We examine this more closely in Sec. V C.

V. A CLOSER LOOK AT THE ITERATIVE DONOHO-JOHNSTONE THRESHOLD

Separating a turbulent flow into coherent and incoherent components by wavelet transformation requires careful consideration of the threshold used in the filter operation. CVE estimates the variance



FIG. 1. Logarithm of the probability density of the velocity $P(u_x)$ in (a) and vorticity $P(\omega_x)$ in (b). The coherent (dashed) and incoherent (dotted-dashed) components of the original (solid) Taylor-Green flow were computed using the Coifman12 wavelet in the CVE analysis (iterative Donoho-Johnstone threshold applied to vorticity magnitude). Dotted curves indicate Gaussian probability density functions (PDFs) with the same mean and variance. Insets show incoherent flow velocity and vorticity PDFs and the Gaussian fits over a narrower range of values. The flow is quite isotropic with nearly identical PDFs for the *y* and *z* velocity, though the *z* velocity is more Gaussian with somewhat smaller variance.

of the noise as that of the vorticity, and applies an iterative scheme⁵ to estimate the universal threshold⁴ based on convergence of the incoherent vorticity variance. Often that convergence is approximated by the variance after a single iteration^{8–10} or the variance of the total vorticity itself (no iteration).^{3,16} The fully iterated threshold would yield optimal de-noising if the flow vorticity were indeed composed of coherent signal and incoherent noise and if the latter were both Gaussianly distributed and spatially uncorrelated. If such were the case, one would also expect the incoherent helicity distribution to reflect random velocity and vorticity vector orientations and the incoherent kinetic energy to scale as k^2 .

A. Is the incoherent vorticity Gaussianly distributed?

We tested the hypothesis that each vector component of the incoherent vorticity is independently Gaussianly distributed using the Pearson χ^2 and the Anderson-Darling tests.^{17–19} We took the model



FIG. 2. (Color) Relative kinetic helicity distribution in the (a) Taylor-Green and (b) ABC flows. Black curves plot values for the original flow (solid) and the coherent (dashed) and incoherent (dotted-dashed) components, the later found using the Coifman12 wavelet in the CVE analysis (iterative Donoho-Johnstone threshold applied to the vorticity vector magnitude). Red and blue curves show the same components obtained using the most Gaussian vorticity and 60% compression thresholds, respectively. Green curves plot values obtained when applying the iterative Donoho-Johnstone threshold to individual vorticity component amplitudes. Insets display incoherent results over a limited range, and dotted curves in inset (a) indicate helicity distribution of randomized vector components (Sec. V B).

distribution to be Gaussian with the same mean and variance as the incoherent data. To make the binned χ^2 test less sensitive to outliers, data that were further than $\pm 4.5\sigma$ from the mean and thus corresponding to a model prediction of less than 5.5 points within the bin was excluded. The Anderson-Darling test is more robust to outliers and only values where the cumulative density function of the model Gaussian distribution had value zero or one to machine precision were omitted. Validation tests with 1024³ Gaussianly distributed random numbers in place of the incoherent flow vorticity components confirmed with better than 99% confidence that in these test cases the hypothesis could not be dismissed. As a secondary validation criteria we confirmed that the probabilities-to-exceed in the random number cases were uniformly distributed.

We performed these tests on the incoherent vorticity identified using the iterative Donoho-Johnstone threshold applied to the vorticity magnitude (standard CVE analysis) in solutions with both flow forcings and employing all three wavelets. The results of both tests indicate that the



FIG. 3. (Color) Kinetic energy spectra of the (a) Taylor-Green and (b) ABC flows. Black curves for the original flow (solid), and coherent (dashed), and incoherent (dotted-dashed) components, the later determined using the Coifman12 wavelet in the CVE analysis (iterative Donoho-Johnstone threshold applied to the vorticity vector magnitude). Red and blue curves show the same components obtained using the most Gaussian vorticity and 60% compression thresholds, respectively. Green curves for values obtained by applying the iterative Donoho-Johnstone threshold to individual vorticity component amplitudes. Note that the wavelet decomposition introduces power above the Orszag frequency k_{max} into both the coherent and incoherent components (Sec. III), but that these sum to zero in amplitude. Fiducial $k^{-5/3}$ and k^2 lines shown for reference.

incoherent flow vorticity is in all cases significantly non-Gaussianly distributed, with the χ^2 test yielding zero probability-to-exceed to machine precision. The measured reduced χ^2 and the Anderson-Darling test statistic A^2 (W_n^2 in Refs. 18 and 19) have values of ~1100 and ~10⁶, respectively. The Gaussian distribution is rejected at the 1% significance level when these values exceed 1.02 and 1.09 for our binned χ^2 and Anderson-Darling tests, respectively. We note that while the incoherent velocity appears by eye to be quite Gaussianly distributed, careful evaluation indicates that it too shows non-Gaussianity ($\chi^2 \sim 300$ and $A^2 \sim 5 \times 10^5$, respectively), though less than the incoherent vorticity. Here we focus on the Gaussianity of the incoherent vorticity rather than the velocity because it is that quantity which underlies the applicability of the iterative Donoho-Johnstone threshold in CVE, though the later may be more important when using CVE in turbulence modeling.



FIG. 4. (Color) In (a), the Anderson-Darling test statistic A^2 measuring the Gaussianity of the incoherent component of the flow as a function of compression, and in (b) A^2 as a function of threshold value A_{DJ} . Filled and empty symbols indicate analysis on the Taylor-Green and ABC solutions, respectively. The incoherent component was extracted using the Haar (circles), Coifman12 (squares), and Coifman30 (triangles) wavelets. Black curves highlight Coifman12 and Haar analysis of the Taylor-Green flow. The incoherent A^2 values obtained for thresholds (applied to vorticity vector magnitude of the Coifman12 wavelet decomposition) yielding the most Gaussian incoherent component are shown in red and those yielding 60% compression in blue (60% compression symbols for Taylor-Green and ABC flows directly overlap). The incoherent A^2 values obtained using the iterative Donoho-Johnstone threshold applied to the individual vorticity amplitudes are shown by the six disconnected points with highest compression on the right of (a) without crosses. Symbols with superimposed crosses indicate results for incoherent flows determined by application of the single iteration threshold to the vorticity vector magnitude, as done in previous studies.

Employing the same hypothesis tests, we examined a range of arbitrary wavelet amplitude thresholds. Compression near 80% yielded the most Gaussianly distributed (by either test) incoherent vorticity, with only weak sensitivity to the wavelet employed or the simulation solution studied (Figure 4(a)), though these most Gaussian distributions remain statistically non-Gaussian with very large A^2 values and zero probability-to-exceed reduced χ^2 values. We also tested the Gaussianity

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025102-10 Lord et al.

of the incoherent distributions after thresholding the individual vorticity components rather than the vorticity vector magnitude. For any given compression rate, filtering the individual vorticity components yields more Gaussianly distributed (though still significantly non-Gaussian) incoherent vorticity values than does filtering based on the vorticity vector magnitude. However, since, for a given threshold value, the overall the compression is greater when the filter is based on vector component amplitudes than it is when based on vector magnitude, the Gaussianity of the incoherent vorticity is comparably less when the fully iterated threshold is applied to the vorticity vector components than when the same threshold is applied to the vector magnitude (Figure 4(a)).

We note that, while the Gaussianity of the incoherent flow monotonically increases with decreasing compression down to 80%, it then somewhat counterintuitively decreases again from the minimum A^2 value as even lower threshold values are employed (Figure 4). We understand this as follows: at very low compression ratios the incoherent vorticity component is composed of the few wavelets of lowest amplitude and its distribution is strongly peak at zero since many nearly zero vorticity values contribute to the probability density. As the compression ratio increases and more wavelets are added to the incoherent component, the distribution "rounds out," with wavelets of many scales randomly contributing. A minimum A^2 value is reached, before, with further compression, the non-Gaussian nature of the original vorticity distribution dominates the incoherent component, with the two becoming one and the same at 100% compression. Interestingly, and somewhat unexpectedly, near the most Gaussian value the curves collapse more completely when A^2 is plotted against threshold value itself (Figure 4(b)) than when it is plotted against the compression achieved (Figure 4(a)). While the compression achieved for a given threshold depends on the details of wavelet employed, the Gaussianity of the noise seems to depend only on the threshold value itself.

B. Does the incoherent flow helicity indicate random vector orientations?

The existence of a wavelet filter that yields a more Gaussianly distributed noise component than that found via the iterative Donoho-Johnstone scheme, suggests that the conditions necessary for the successful application of the universal threshold may not be met in these turbulence simulation solutions because the incoherent component extracted by the filter is non-Gaussian. This suggests that the incoherent component may similarly retain correlations which perhaps persist to very low amplitudes in the turbulent flow. One important correlation is that between the velocity and vorticity vector orientations.

Figure 2(a) shows that the kinetic helicity distribution of the incoherent component of the Taylor-Green flow peaks at h = 0 and has opposite curvature to that of the original, as it also does in previous work.^{2,3,12} Vectors of random magnitude and orientation would show uniformly distributed helicity (with normalized P(h) = 0.5). The incoherent helicity distribution differs from this, though scrambling the individual incoherent vorticity and velocity vectors by randomly sampling their components produces helicity distributions that are close to uniform (dotted curves in inset of Figure 2(a) indicating that it is the helicity vector direction that is to some degree preserved by the incoherent flow. Thus, application of the threshold filter to individual vorticity component amplitudes rather than the vector magnitude yields an incoherent helicity distribution closest to that of randomly oriented vectors because such component filtering serves to scramble the vorticity and velocity vector directions. Without such scrambling, as when the threshold filter is applied to the vorticity vector magnitudes (the usual CVE procedure), a residual of the original flow helicity contaminates in the incoherent component. This is true for all filter thresholds, with no wavelet decomposition of the Taylor-Green flow yielding strictly randomly oriented vorticity and velocity vectors, and a consequent uniform helicity distribution, in the incoherent flow. Analysis of the ABC flow (Figure 2(b)) confirms this result. Net helicity is introduced into the ABC flow via the driving, and the incoherent component in all cases reflects this bias, albeit very weakly at 60% compression.

C. Does the incoherent kinetic energy scale as k^2 ?

A spatially uncorrelated three-dimensional random field (equal power in all spectral modes independent of direction) necessitates power scaling as k^2 . This scaling is reported for the

incoherent flow component of previously published wavelet decompositions.^{2,3,9,12} We find it to hold only over a very limited range of high wavenumbers and then only when the each component of the vorticity is filtered independently, not when the filtering is applied to the vorticity vector magnitude, though it is the later procedure which is followed in previous studies. In our studies, filtering by the vorticity vector magnitude yields much steeper incoherent kinetic energy spectra (Figure 3). This likely results because, it is only by filtering the vorticity components separately that we achieve compression rates comparable to those previously published, and it is this overall compression that largely determines low wavenumber contributions to the incoherent component. We have computed the single iteration incoherent energy spectra for both the TG and ABC flows and these show flatter spectra, akin to those reported by previous authors, though some uncertainty remains as published fully iterated results do not show the steeper slope that we find [cf. Ref. 9].

The simulations studied here were forced coherently, with turbulence developing from the instability of the large-scale flow driven with a well defined geometry. Thus, the steeper incoherent power spectrum observed in our work alternatively may reflect the coherent nature of our low wave number driving, with that coherence partially destroyed when the filter is applied to individual component amplitudes, flattening the noise spectrum toward k^2 . However, we note that previous CVE studies, which also show the flatter spectrum, examined both run-down and forced turbulence simulation solutions resulting from a range of forcing schemes. It is thus likely that it is the high compressions achieved in those studies and in our component filtering analysis, rather than the particulars of the flow forcing, that underly the enhanced low wavenumber power spectrum observed. It is unclear, therefore, whether the limited k^2 spectra observed in previous studies necessarily implies the existence of a spatially uncorrelated random component in the flow.

VI. SPATIAL AND TEMPORAL CORRELATIONS

The coherence of our driving scheme is also reflected in persistent spatial correlations evident in the incoherent component of the Taylor-Green and ABC flows even at very low compressions. As an example, the Taylor-Green forcing (Eq. (3)) has a cosine form in the *z* direction, with alternating regions of oppositely signed forcing producing regions of high vorticity at the interfaces. The autocorrelation of the enstrophy in that direction shows these alternating regions clearly in both the coherent and incoherent components (Figure 5(a)). In fact, when employing the iterative Donoho-Johnstone threshold the large scale correlations have a larger amplitude in the incoherent flow component than they do in the original flow because smaller scale fluctuations contribute less to the correlation measure. At lower compressions the signature of the large scale forcing is reduced but persists. We note that the spatial autocorrelation plot in Figure 5(a) shows two curves for each of the incoherent components. This reflects oscillations in the incoherent component at the Nyquist frequency, not seen in the original flow, due to enhanced power above the Orszag frequency k_{max} as a result of the wavelet filtering (see Sec. III).

Understanding the temporal correlation of the incoherent component is important to efforts aimed at using CVE filtering and incoherent component modeling as simulation tools. We find such temporal correlations to be less pronounced than the spatial correlations. We computed the temporal correlation of one vorticity component between 40 volumetric snapshots spanning 0.4 turnover times of the Taylor-Green flow (the turnover time here defined in terms of the integral length scale and the root-mean-square velocity). The iterative Donoho-Johnstone filter threshold was very stable over these snapshots. The number of iterations required for convergence varied between 32 and 38, and the threshold values differed by at most 1.3% between any two snapshots. A full width half maximum de-correlation time of ~0.056 was found for both the original flow and coherent component while one of ≤ 0.01 was obtained for the incoherent component. Slightly shorter temporal correlation times were found for lower compressions, but even the iterative Donoho-Johnstone scheme applied to the individual vorticity amplitudes (maximum compression) yielded an incoherent flow with very short temporal correlation (Figure 5(b)).



FIG. 5. (Color) In (a), spatial autocorrelation ρ_z of the Taylor-Green enstrophy as a function of the spatial lag Δz , and in (b), the temporal correlation ρ_τ of Taylor-Green vorticity ω_x as a function of temporal lag τ (vorticity chosen here only to reduce the computational cost of time series analysis). Black curves for the original flow (solid) and coherent (dashed) and incoherent (dotted-dashed) components, the later determined using the Coifman12 wavelet in the CVE analysis (iterative Donoho-Johnstone threshold applied to the vorticity vector magnitude). Red and blue curves show results for the same components obtained using the most Gaussian vorticity and 60% compression thresholds, respectively, and in green, those for components identified using the iterative Donoho-Johnstone threshold applied to the individual vorticity amplitudes. The coherent components (dashed lines) in (a) underlie the solid curve and are thus hidden from view. The double curve for each of the incoherent components (dotted-dashed lines) in (a) reflects grid oscillation of the incoherent component at the Nyquist frequency, not seen in the original flow, due to enhanced power above the Orszag frequency k_{max} as a result of the wavelet filtering (Sec. III).

VII. CONCLUSION

Wavelet filtering promises significant compression of turbulence simulation data and possible modeling schemes based on evolving the coherent flow component only. The coherent flow identified in the CVE analysis shares many properties with the original solutions using only a small fraction of the wavelet coefficients. A scheme which evolves these coefficients while modeling the remaining

incoherent contribution would yield a tremendous decrease in computation effort.¹⁶ The difficulty lies in how best to model the incoherent or noise component.

Our results suggest that the incoherent component of forced turbulence, when extracted using an orthonormal wavelet decomposition, cannot be strictly modeled as Gaussian random noise. It retains residual vector correlations (helicity) found in the original flow and spectral energy distribution and spatial correlations that reflect the forcing function. These difficulties can be diminished by reducing the threshold criterion, thereby reducing the compression achieved, but they persist at some level for all thresholds we examined. The turbulent flows we examined (forced coherently at large scale as a Taylor-Green or ABC flow) cannot be conceptually separated into coherent signal and incoherent noise with distinctly different properties. The filtering operation always to some extent removes flow in addition to any noise component that may be present. The short temporal correlation time of the incoherent component does, however, suggest that if, despite these difficulties, a model of the low amplitude coefficients can be developed, that model could be based on the current state of the coherent flow, independent of its evolution.

Finally, an item of significant interest to modeling efforts is the flow divergence introduced by CVE filtering. Previous authors have pointed out that the orthogonal wavelet transform does not commute with the divergence operator and thus CVE filtering introduces spurious divergence into the coherent vorticity field.⁹ We found, as previous authors, that the divergence introduced into the coherent vorticity is small, and that introduced into the coherent velocity is comparable to the precision of the scheme used to compute the divergence itself. Specifically, for the coherent component, we find average values of $\nabla \cdot \boldsymbol{\omega}$ and $\nabla \cdot \boldsymbol{u}$, normalized by their mean magnitudes $|\boldsymbol{\omega}|$ and $|\boldsymbol{u}|$, of 10% and 0.08%, respectively when applying the Coifman12 fully iterated Donoho-Johnstone threshold to the vorticity vector magnitude, 14% and 0.06%, when basing that threshold on the first iteration as in previous studies, and 14% and 0.07% when applying the fully iterated Donoho-Johnstone threshold to the individual vector components. Careful and complete study of the sensitivity of these results to the wavelet type, filtering scheme, and compression achieved is left for future work.

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025102-14 Lord et al.

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